# Low-Power Single/Dual-Supply Dual Comparator with Reference

## FEATURES

- Ultra-Low Quiescent Current: 4µA (max), Both Comparators plus Reference
- Single or Dual Power Supplies: Single: +2.5V to +11V Dual: ±1.25V to ±5.5V
- Input Voltage Range Includes Negative Supply
- ♦ 7µs Propagation Delay
- Push-pull TTL/CMOS-Compatible Outputs
- ◆ Crowbar-Current-Free Switching
- Continuous Source Current Capability: 40mA
- ♦ Internal 1.182V ±0.75% Reference
- Adjustable Hysteresis
- ♦ 8-pin MSOP Package

## **APPLICATIONS**

Threshold Detectors Window Comparator Level Translators Oscillator Circuits Battery-Powered Systems

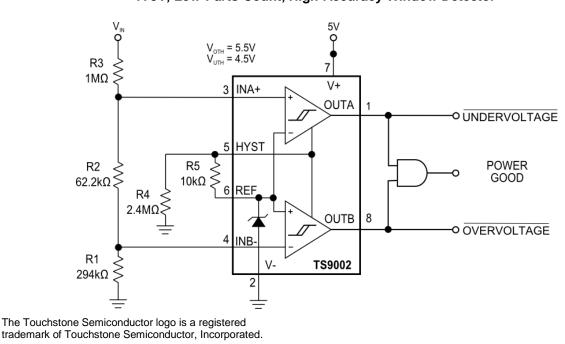
### DESCRIPTION

The TS9002 low-voltage, micropower dual analog comparator is form-factor identical to the MAX923 analog comparator with improved electrical specifications. Ideal for 3V or 5V single-supply applications, the TS9002 draws 11% lower supply current with a 25%-better initial accuracy reference voltage. The TS9002 joins Touchstone's TS9001-1/2 analog comparators in the "NanoWatt Analog<sup>TM</sup>" high performance analog integrated circuits portfolio. The TS9002 can operate from single +2.5V to +11V supplies or from  $\pm 1.25V$  to  $\pm 5.5V$  dual supplies.

The TS9002 exhibits an input voltage range from the negative supply rail to within 1.3V of the positive supply rail. In addition, its push-pull output stage is TTL/CMOS compatible and capable of sinking and sourcing current. It also incorporates an internal 1.182V  $\pm 0.75\%$  voltage reference. Without complicated feedback configurations and only requiring two additional resistors, adding external hysteresis via a separate pin is available on the TS9002's HYST pin.

The TS9002 is fully specified over the -40°C to +85°C temperature range and is available in a 8-pin MSOP package.

#### TYPICAL APPLICATION CIRCUIT A 5V, Low-Parts-Count, High-Accuracy Window Detector





## **ABSOLUTE MAXIMUM RATINGS**

Supply Voltage (V+ to V-, V+ to V	GND, GND to V-)0.3V, +12V
Voltage Inputs	
(IN+, IN-)	(V+ + 0.3V) to (V 0.3V)
Output Voltage	
REF	(V+ + 0.3V) to (V 0.3V)
OUT	(V+ + 0.3V) to (V 0.3V)
Output Current	
REF	20mA
OUT	40mA

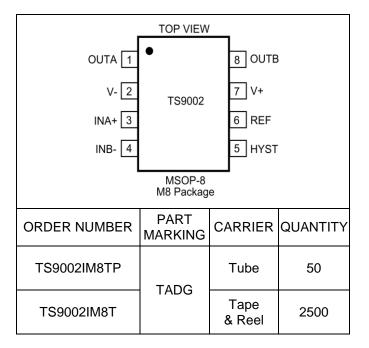
Output Short-Circuit Duration (V+ ≤ 5.5V) .....Continuous

Continuous Power Dissipation ( $T_A = +70^{\circ}C$ )

8-Pin MSOP (derate 4.1mW/°C above +70°	°C)330mW
Operating Temperature Ranges	40°C to +85°C
Storage Temperature Range	65°C to +150°C
Lead Temperature (soldering, 10s)	+300°C

Electrical and thermal stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other condition beyond those indicated in the operational sections of the specifications is not implied. Exposure to any absolute maximum rating conditions for extended periods may affect device reliability and lifetime.

## PACKAGE/ORDERING INFORMATION



Lead-free Program: Touchstone Semiconductor supplies only lead-free packaging.

Consult Touchstone Semiconductor for products specified with wider operating temperature ranges.



## **ELECTRICAL CHARACTERISTICS – 5V OPERATION**

V+ = 5V, V- = GND = 0V;  $T_A$  = -40°C to +85°C, unless otherwise noted. Typical values are at  $T_A$  = +25°C. See Note 1.

PARAMETER	CONDITIONS			MIN	TYP	MAX	UNITS		
POWER REQUIREMENTS									
Supply Voltage Range					2.5		11	V	
Supply Current	IN+ = IN- + 100mV	цус	HYST = REF $T_A = +2$			2.6	4	μA	
,	IIN + = IIN - + 100 MV HY		-40°C to +85°C				5.2	μΑ	
COMPARATOR									
Input Offset Voltage	V <sub>CM</sub> = 2.5V		$T_A = +25^{\circ}C$				±3.5	mV	
input onset voltage			-40°C to +85°C				±10		
Input Leakage Current (IN-, IN+)	IN+ = IN- = 2.5V		$T_A = +25^{\circ}C$			±0.01	±2	nA	
			-40°C to +85°C			±0.01	±5	nA	
Input Leakage Current (HYST)			$T_A = +25^{\circ}C$			±0.02		nA	
			-40°C to	) +85°C		±0.02		nA	
Input Common-Mode Voltage Range					V-		V+ – 1.3V	V	
Common-Mode Rejection Ratio	V- to (V+ – 1.3V)				0.1	1	mV/V		
Power-Supply Rejection Ratio	V+ = 2.5V to 11V					0.1	1	mV/V	
Output Voltage Noise	100Hz to 100kHz					20		$\mu V_{RMS}$	
Hysteresis Input Voltage Range					REF- 0.05V		REF	V	
Response Time	$T_A = +25^{\circ}C$ , 100pF load		Overdriv	/e = 10 mV		17		μs	
(High-to-Low Transition)				/e = 100 mV		7			
Response Time	T <sub>A</sub> = +25°C, 100pF	beol	Overdriv	/e = 10 mV		17		μs	
(Low-to-High Transition)	1 <sub>A</sub> = +23 C, 100pi	LUau	Overdrive = 100 mV			7			
Output High Voltage				$I_{OUT} = 17 mA$	V+-0.4			V	
Output Low Voltage	-40°C to +85°C; I <sub>OUT</sub> = 1.8mA					GND + 0.4	V		
	Dual Supply $-40^{\circ}$ C to $+85^{\circ}$ C; $I_{OUT} = 1.8$ mA			$I_{OUT} = 1.8 \text{mA}$			V-+0.4	V	
REFERENCE			_						
Reference Voltage			$T_{A} = +25$		1.173	1.182	1.191	V	
			-40°C to	) +85°C	1.164		1.199	v	
Reference Line Regulation	2.5V ≤ (V+ - V-) ≤ 11V		$T_A = +25^{\circ}C$			0.25		mV/V	
Source Current	ΔVREF = 1%		$T_{A} = +25$		20	25		μA	
			-40°C to	) +85°C	6			μΑ	
Sink Current	۵VREF = 1%		$T_{A} = +25$		10	15		μΑ	
		-40		) +85°C	4				
Output Voltage Noise	100Hz to 100kHz					100		$\mu V_{RMS}$	



## **ELECTRICAL CHARACTERISTICS – 3V OPERATION**

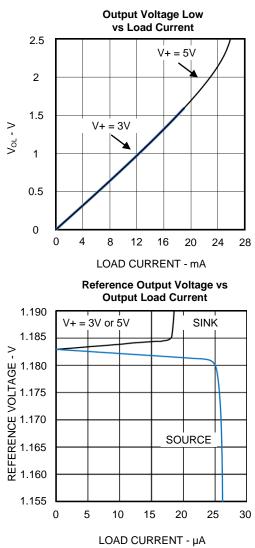
V+ = 3V, V- = GND = 0V;  $T_A$  = -40°C to +85°C, unless otherwise noted. Typical values are at  $T_A$  = +25°C. See Note 1.

PARAMETER	CONDITIONS			MIN	TYP	MAX	UNITS	
POWER REQUIREMENTS				· ·				
Supply Current	IN+ = IN- + 100mV	HYST = REF	$T_{A} = +25^{\circ}C$		2	3.8	μA	
	10+=10-+10000	ITISI = REF	-40°C to +85°C			5.3		
COMPARATOR		-						
Input Offset Voltage	V <sub>CM</sub> = 1.5V	$T_A = +2$	$T_A = +25^{\circ}C$			±3.5	mV	
input Onset Voltage	$v_{CM} = 1.5v$	-40°C 1	-40°C to +85°C			±10		
Input Leakage Current (IN-, IN+)	IN+ = IN- = 1.5V	$T_A = +2$	25°C		±0.01	±2	nA	
Input Leakage Current (IN-, IN+)	110 + = 10 - = 1.5V	-40°C 1	o +85°C		±0.01	±5	nA	
Input Leakage Current (at HYST Pin)		$T_A = +2$	25°C		±0.02		nA	
Input Leakage Current (at 11131 Fill)		-40°C 1	o +85°C		±0.02		nA	
Input Common-Mode Voltage Range				V-		V+ – 1.3V	V	
Common-Mode Rejection Ratio	V- to (V+ – 1.3V)				0.1	1	mV/V	
Power-Supply Rejection Ratio	V + = 2.5V  to  11V				0.1	1	mV/V	
Output Voltage Noise	100Hz to 100kHz				20		$\mu V_{RMS}$	
Hysteresis Input Voltage Range				REF- 0.05V		REF	V	
Response Time	T <sub>A</sub> = +25°C, 100pF I	Overdr	ive = 10 mV		17		μs	
(High-to-Low Transition)	$T_A = +25 \text{ C}, 100 \text{ pr}$	Overdr	ive = 100 mV		7			
Response Time	T <sub>A</sub> = +25°C, 100pF l	Overdr	ive = 10 mV		17		μs	
(Low-to-High Transition)	$T_A = +25 \text{ C}, 100 \text{ pr}$	Overdr	ive = 100 mV		7			
Output High Voltage		-40°C to +85°C	; I <sub>OUT</sub> = 10mA	V+-0.4			V	
Output Low Voltage		-40°C to +85°C	; I <sub>OUT</sub> = 1.8mA			GND + 0.4	V	
Oulput Low Voltage	Dual Supply					V- + 0.4	V	
REFERENCE								
Reference Voltage		$T_A = +2$	25°C	1.173	1.182	1.191	V	
Reference voltage			o +85°C	1.164		1.199	v	
Reference Line Regulation	2.5V ≤ (V+ - V-) ≤ 5V	$/$ $T_A = +2$	25°C		0.25		mV/V	
Source Current	ΔVREF = 1%	$T_{A} = +2$	25°C	20	25		μA	
	$\Delta VIXEF = 170$	-40°C	o +85°C	6				
Sink Current	۵VREF = 1%	$T_{A} = +2$	25°C	10	15		μA	
	4VKEF = 1%	-40°C	o +85°C	4				
Output Voltage Noise	100Hz to 100kHz				100		$\mu V_{RMS}$	

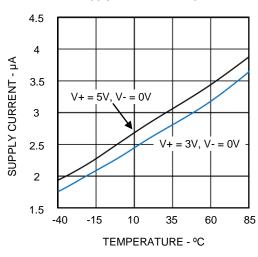
**Note 1:** All specifications are 100% tested at  $T_A = +25^{\circ}$ C. Specification limits over temperature ( $T_A = T_{MIN}$  to  $T_{MAX}$ ) are guaranteed by device characterization, not production tested.

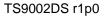
## TYPICAL PERFORMANCE CHARACTERISTICS

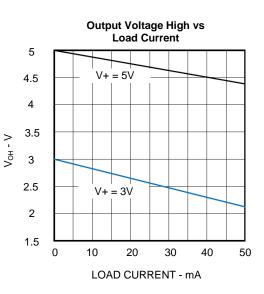
 $V_{+} = 5V$ ;  $V_{-} = GND$ ;  $T_{A} = +25^{\circ}C$ , unless otherwise noted.



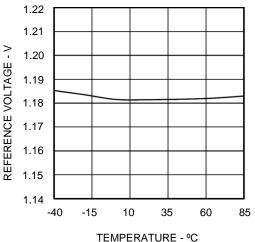
Supply Current vs Temperature



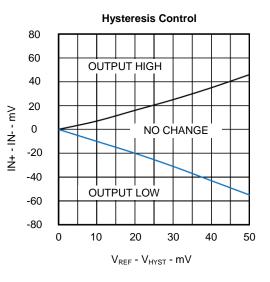




**Reference Voltage vs Temperature** 



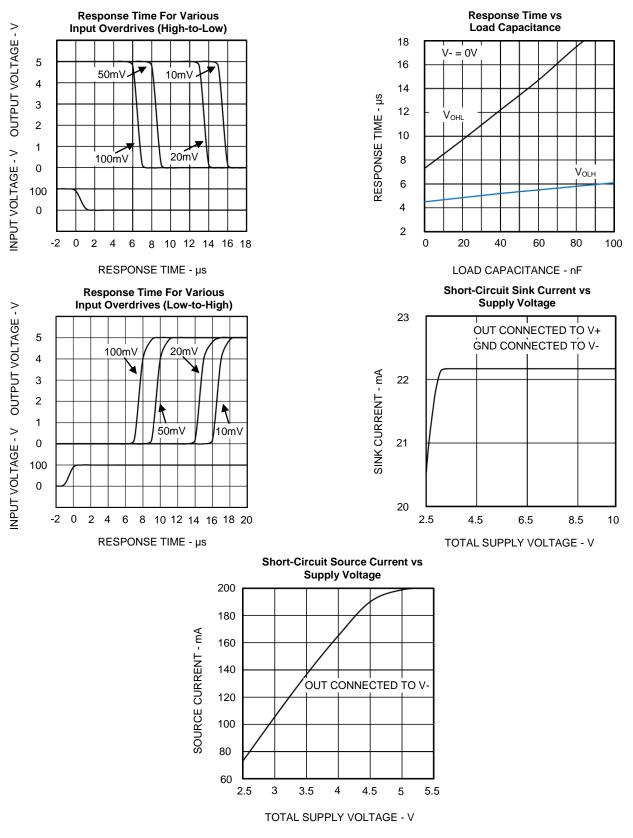
IEWFERATORE -





## **TYPICAL PERFORMANCE CHARACTERISTICS**

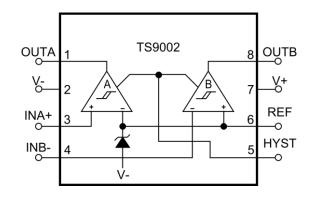
 $V_{*}$  = 5V;  $V_{\cdot}$  = GND;  $T_{A}$  = +25°C, unless otherwise noted.





TS9002 MSOP-8	NAME	FUNCTION			
1	OUTA	Comparator A Output. Sinks and sources current. Swings from V+ to V			
2	V-	Negative Supply Voltage. Connect to ground for single-supply operation.			
3	INA+	Comparator A Noninverting Input			
4	INB-	Comparator B Inverting Input			
5	HYST	Hysteresis Input. Connect to REF if not used. Input voltage range is from VREF to (VREF - 50mV).			
6	REF	1.182V Reference Output with respect to V			
7	V+	Positive Supply Voltage			
8	OUTB	Comparator B Output. Sinks and sources current. Swings from V+ to V			

## **BLOCK DIAGRAM**



## THEORY OF OPERATION

The TS9002 dual, low-voltage, micropower analog comparator provides excellent flexibility and performance while sourcing continuously up to 40mA of current. The TS9002 draws less than  $5.5\mu$ A (total) over temperature for both comparators, including the reference. It also exhibits an input offset voltage of  $\pm 3.5$ mV, and has an on-board  $\pm 1.182$ V  $\pm 0.75\%$  voltage reference. To minimize glitches that can occur with parasitic feedback or a less than optimal board layout, the design of the TS9002 output stage is optimized to eliminate crowbar glitches as the output switches. To minimize current consumption while providing flexibility, TS9002 has an on-board HYST pin in order to add additional hysteresis.

#### **Power-Supply and Input Signal Ranges**

The TS9002 can operate from a single supply voltage range of +2.5V to +11V, provides a wide common mode input voltage range of V- to V+-1.3V, and accepts input signals ranging from V- to V+ - 1V. The inputs can accept an input as much as 300mV above and below the power supply rails without damage to the part. The TS9002 is TTL compatible with a single +5V supply.

#### **Comparator Output**

The output design of the TS9002 can source and sink more than 40mA and 5mA, respectively, while simultaneously maintaining a quiescent current less

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than  $3\mu$ A. If the power dissipation of the package is maintained within the max limit, the output can source pulses of 100mA of current with V+ set to +5V. In an effort to minimize external components needed to address power supply feedback, the TS9002 output does not produce crowbar switching current as the output switches. At a power supply voltage of 3V, the propagation delay of the TS9002 is 6µs when the output switches from high-to-low and low-to-high.

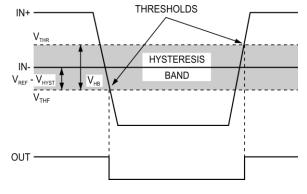
#### Voltage Reference

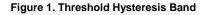
The TS9002 has an on-board +1.182V voltage reference with an accuracy of  $\pm 0.75\%$ . The REF pin is able to source and sink 20µA and 10µA of current,

### **APPLICATIONS INFORMATION**

#### Hysteresis

As a result of circuit noise or unintended parasitic feedback, many analog comparators often break into oscillation within their linear region of operation especially when the applied differential input voltage approaches 0V (zero volt). Externally-introduced hysteresis is a well-established technique to stabilizing analog comparator behavior and requires external components. As shown in Figure 1, adding comparator hysteresis creates two trip points: V<sub>THR</sub> (for the rising input voltage) and  $V_{THF}$  (for the falling input voltage). The hysteresis band ( $V_{HB}$ ) is defined as the voltage difference between the two trip points. When a comparator's input voltages are equal, hysteresis effectively forces one comparator input to move quickly past the other input, moving the input out of the region where oscillation occurs. Figure 1 illustrates the case in which an IN- input is a fixed







respectively. The REF pin is referenced to V- and it should not be bypassed.

#### Noise Considerations

Noise can play a role in the overall performance of the TS9002. Despite having a large gain, if the input voltage is near or equal to the input offset voltage, the output will randomly switch HIGH and LOW. As a result, the TS9002 produces a peak-to-peak noise of about  $0.3mV_{PP}$  while the reference voltage produces a peak-to-peak noise of about  $1mv_{PP}$ . Furthermore, it is important to design a layout that minimizes capacitive coupling from a given output to the reference pin as crosstalk can add noise and as a result, degrade performance.

voltage and an IN+ is varied. If the input signals were reversed, the figure would be the same with an inverted output. Hysteresis can be generated with two external resistors using positive feedback as shown in Figure 2. Resistor R1 is connected between REF and HYST and R2 is connected between HYST and V-. This will increase the trip

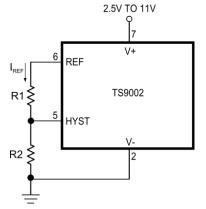


Figure 2. Programming the HYST Pin

point for the rising input voltage,  $V_{THR}$ , and decrease the trip point for the falling input voltage,  $V_{THF}$ , by the same amount. If no hysteresis is required, connect HYST to REF. The hysteresis band,  $V_{HB}$ , is voltage across the REF and HYST pin multiplied by a factor of 2. The HYST pin can accept a voltage between REF and REF-50mV, where a voltage of REF-50mV generates the maximum voltage across R1 and thus, the maximum hysteresis and hysteresis band of 50mV and 100mV, respectively. To design the circuit for a desired hysteresis band, consider the equations below to acquire the values for resistors R1 and R2:



R1 = 
$$\frac{V_{HB}}{(2 \times I_{REF})}$$
  
R2 =  $\frac{1.182 - \frac{V_{HB}}{2}}{1.182 - \frac{V_{HB}}{2}}$ 

where IREF is the primary source of current out of the reference pin and should be maintained within the maximum current the reference can source. It is safe to maintain the current within 20µA. It is also important to ensure that the current from reference is much larger than the HYST pin input current. Given  $R2 = 2.4M\Omega$ , the current sourced by the reference is 0.5µA. This allows the hysteresis band and R1 to be approximated as follows:

 $R1(k\Omega) = V_{HB}(mv)$ 

Note the hysteresis is both the same for comparators.

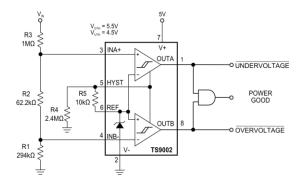
#### **Board Layout and Bypassing**

While power-supply bypass capacitors are not typically required, it is good engineering practice to use 0.1µF bypass capacitors close to the device's power supply pins when the power supply impedance is high, the power supply leads are long, or there is excessive noise on the power supply traces. To reduce stray capacitance, it is also good engineering practice to make signal trace lengths as short as possible. Also recommended are a ground plane and surface mount resistors and capacitors.

#### Window Detector

The schematic shown in Figure 3 is for a 4.5V undervoltage threshold detector and a 5.5V overvoltage threshold detector using the TS9002. Resistor components R1, R2, and R3 can be selected based on the threshold voltage desired while resistors R4 and R5 can be selected based on the hysteresis desired. Adding hysteresis to the circuit will minimize chattering on the output when the input voltage is close to the trip point. OUTA and OUTB generate the active low undervoltage indication and active-low overvoltage indication, respectively. If both OUTA and OUTB signals are ANDed together, the resulting output of the AND gate is an active-high, power-good signal. To design the circuit, the following procedure needs to be followed:

1. As described below, determine the desired hysteresis and select resistors R4 and R5 accordingly. This circuit has ±5mV of hysteresis at the input where the input voltage V<sub>IN</sub> will appear larger due to the input resistor divider.



#### Figure 3. Window Detector

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- 2. Choosing R1. As the leakage current at the INB- pin is less than 1nA, the current through R1 should be at least 100nA to minimize offset voltage errors caused by the input leakage current. Values within 100kΩ and  $1M\Omega$  are recommended. In this example, a 294kO, 1% standard value resistor is selected for R1.
- 3. Calculating R2 + R3. As the input voltage V<sub>IN</sub> rises, the overvoltage threshold should be 5.5V. Choose R2 + R3 as follows:

R1 + R3 = R1 x 
$$\left(\frac{V_{OTH}}{V_{REF}+V_{HYS}}-1\right)$$
  
= 294k $\Omega$  x  $\left(\frac{5.5V}{1.182V+5mV}-1\right)$   
= 1.068M $\Omega$ 

4. Calculating R2. As the input voltage V<sub>IN</sub> falls, the undervoltage threshold should be 4.5V. Choose R2 as follows:

R2 = (R1 + R2+ R3) x 
$$\frac{(V_{REF}-V_{HYS})}{V_{UTH}}$$
 - 294k  
= (294k $\Omega$  + 1.068M $\Omega$ ) x  $\frac{(1.182V-5mV)}{4.5}$  - 294k  
= 62.2k $\Omega$ 

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In this example, a  $61.9k\Omega$ , 1% standard value resistor is selected for R2.

5. Calculating R3.

R3 = (R2 + R3) - R2= 1.068M $\Omega$  - 61.9k $\Omega$ 

= 1.006MΩ

In this example, a 1M $\Omega$ , 1% standard value resistor is selected for R3.

6. Using the equations below, verify all resistor values selected:

$$V_{OTH} = (V_{REF} + V_{HYS}) x \frac{(R1 + R2 + R3)}{R1}$$

= 5.474V

$$V_{OTH} = (V_{REF} - V_{HYS}) \times \frac{(R1 + R2 + R3)}{(R1+R2)}$$

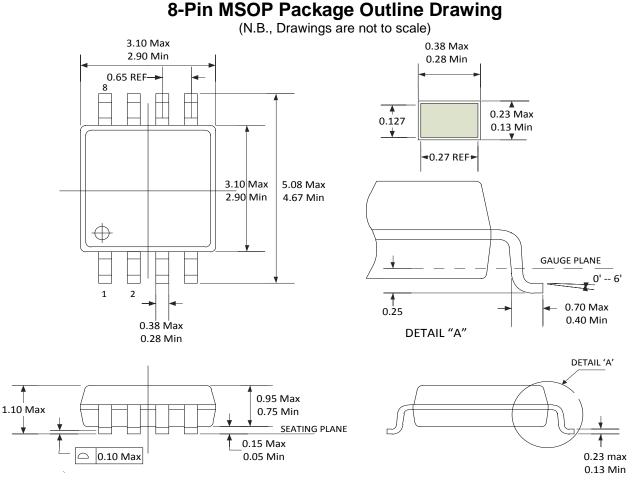
= 4.484V

Where the hysteresis voltage is given by:

 $V_{HYS} = V_{REF} \times \frac{R5}{R4}$ 

PACKAGE OUTLINE DRAWING

Touchstone



NOTE:

- 1. PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS.
- 2. PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTUSIONS.
- 3. CONTROLLING DIMENSION IN MILIMETERS.
- 4. THIS PART IS COMPLIANT WITH JEDEC MO-187 VARIATIONS AA
- 5. LEAD SPAN/STAND OFF HEIGHT/COPLANARITY ARE CONSIDERED AS SPECIAL CHARACTERISTIC.

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