#### MAX17574

# 4.5V to 60V, 3A, High-Efficiency, Synchronous Step-Down DC-DC Converter with Internal Compensation

### **General Description**

The MAX17574, high-efficiency, high-voltage, synchronous step-down DC-DC converter with integrated MOSFETs operates over a 4.5V to 60V input. The converter can deliver up to 3A current. Output voltage is programmable from 0.9V to  $90\%V_{IN}$ . The feedback voltage regulation accuracy over -40°C to +125°C is ±0.9%.

The MAX17574 features a peak-current-mode control architecture. The device can be operated in the pulse-width modulation (PWM), pulse-frequency modulation (PFM), or discontinuous-conduction mode (DCM) control schemes. A programmable soft-start feature allows users to reduce input inrush current. The device also incorporates an output enable/undervoltage lockout pin (EN/UVLO) that allows the user to turn on the part at the desired input voltage level. An open-drain RESET pin provides a delayed power-good signal to the system upon achieving successful regulation of the output voltage.

The MAX17574 is available in a 24-pin (4mm x 5mm) TQFN package. Simulation models are available.

## **Applications**

- Industrial Control Power Supplies
- General-Purpose Point-of-Load
- Distributed Supply Regulation
- Base Station Power Supplies
- Wall Transformer Regulation
- High-Voltage, Single-Board Systems

#### **Benefits and Features**

- Reduces External Components and Total Cost
  - · No Schottky-Synchronous Operation
  - Internal Compensation for Any Output Voltage
  - · All-Ceramic Capacitors, Compact Layout
- Reduces Number of DC-DC Regulators to Stock
  - · Wide 4.5V to 60V Input
  - Output Adjustable from 0.9V to 90%V<sub>INI</sub>
  - Delivers up to 3A Current Over Temperature
  - 100kHz to 2.2MHz Adjustable Switching Frequency with External Synchronization
- Reduces Power Dissipation
  - Peak Efficiency > 90%
  - PFM and DCM Modes Enable Enhanced Light-Load Efficiency
  - Auxiliary Bootstrap LDO for Improved Efficiency
  - 2.8µA Shutdown Current
- Operates Reliably in Adverse Industrial Environments
  - · Hiccup Mode Overload Protection
  - · Adjustable Soft-Start and Prebiased Power-Up
  - Built-In Output-Voltage Monitoring with RESET
  - Programmable EN/UVLO Threshold
  - · Monotonic Startup Into Prebiased Load
  - · Overtemperature Protection
  - High Industrial -40°C to +125°C Ambient Operating Temperature Range/-40°C to +150°C Junction Temperature Range

Ordering Information appears at end of data sheet.



### MAX17574

# 4.5V to 60V, 3A, High-Efficiency, Synchronous Step-Down DC-DC Converter with Internal Compensation

### **Absolute Maximum Ratings (Note 1)**

	- 3- ( /		
V <sub>IN</sub> to PGND	0.3V to +65V	PGND to SGND	0.3V to +0.3V
EN/UVLO to SGND	0.3V to +65V	LX Total RMS Current	±5.6A
LX to PGND	0.3V to V <sub>IN</sub> + 0.3V	Output Short-Circuit Duration	Continuous
EXTVCC to SGND	0.3V to +26V	Continuous Power Dissipation (multilayer	Board) ( $T_A = +70^{\circ}C$ ,
BST to PGND	0.3V to +70V	derate 41.7mW/°C above +70°C.)	3333mW
BST to LX	0.3V to +6.5V	Junction Temperature	+150°C
BST to V <sub>CC</sub>	0.3V to +65V	Storage Temperature Range	65°C to +150°C
FB, RESET, SS, MODE/SYNC,		Lead Temperature (soldering, 10s)	+300°C
V <sub>CC</sub> , RT, CF to SGND	0.3V to +6.5V	Soldering Temperature (reflow)	+260°C
FB to SGND	0.3V to +1.5V		

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only; functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device

### **Package Information**

PACKAGE TYPE: 24 TQFN			
Package Code	T2445+1C		
Outline Number	21-0201		
Land Pattern Number	90-0083		
THERMAL RESISTANCE, FOUR-LAYER BOARD (Note 2)			
Junction to Ambient (θ <sub>JA</sub> )	24°C/W		
Junction to Case (θ <sub>JC</sub> )	1.8°C/W		

For the latest package outline information and land patterns (footprints), go to www.maximintegrated.com/packages. Note that a "+", "#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

Note 1: Junction temperature greater than +125°C degrades operating lifetimes.

Note 2: Package thermal resistances were obtained using the MAX17574 evaluation kit.

### **Electrical Characteristics**

 $(V_{IN} = V_{EN/UVLO} = 24V, R_{RT} = 40.2K\Omega (f_{SW} = 500kHz), C_{VCC} = 10\mu F, V_{SGND} = V_{PGND} = V_{MODE/SYNC} = V_{EXTVCC} = 0V, V_{FB} = 1V, LX = SS = CF = RESET = OPEN, V_{BST} to V_{LX} = 5V, T_{A} = -40^{\circ}C$  to 125°C, unless otherwise noted. Typical values are at  $T_{A} = +25^{\circ}C$ . All voltages are referenced to SGND, unless otherwise noted.) (Note 3)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
INPUT SUPPLY (VIN)	•					
Input Voltage Range	V <sub>IN</sub>		4.5		60	V
Input Shutdown Current	I <sub>IN-SH</sub>	V <sub>EN/UVLO</sub> = 0V (shutdown mode)		2.8	4.5	μΑ
	I <sub>Q PFM</sub>	MODE/SYNC = RT = open, EXTVCC = 5V		61		μΑ
Innut Ouissant Current	_	MODE/SYNC = open, EXTVCC = 5V		71		μΑ
Input Quiescent Current	I <sub>Q_DCM</sub>	DCM Mode, V <sub>LX</sub> = 0.1V		1.2	1.8	mA
	I <sub>Q_PWM</sub>	Normal switching mode, F <sub>SW</sub> = 500kHz, V <sub>FB</sub> = 0.8V		14		mA
ENABLE/UVLO (EN)						
EN/UVLO Threshold	V <sub>ENR</sub>	V <sub>EN/UVLO</sub> rising	1.19	1.215	1.26	V
EN/UVLO Threshold	V <sub>ENF</sub>	V <sub>EN/UVLO</sub> falling	1.068	1.09	1.131	V
EN/UVLO Threshold	V <sub>EN-TRUESD</sub>	V <sub>EN/UVLO</sub> falling		0.8		V
EN Input Leakage Current	I <sub>EN</sub>	V <sub>EN/UVLO</sub> = 0V, T <sub>A</sub> = +25°C	-50	0	+50	nA
V <sub>CC</sub> LDO						
V Output Valtage Bange		1mA ≤ I <sub>VCC</sub> ≤ 25mA	4.75	5	5.25	V
V <sub>CC</sub> Output Voltage Range	V <sub>CC</sub>	6V ≤ V <sub>IN</sub> ≤ 60V; I <sub>VCC</sub> = 1mA	4.75	5	5.25	V
V <sub>CC</sub> Current Limit	I <sub>VCC-MAX</sub>	V <sub>CC</sub> = 4.3V, V <sub>IN</sub> = 7V	40	65	130	mA
V <sub>CC</sub> Dropout	V <sub>CC-DO</sub>	V <sub>IN</sub> = 4.5V , I <sub>VCC</sub> = 20mA	4.2			V
V 11VI O	V <sub>CC-UVR</sub>	Rising	4.05	4.2	4.3	V
V <sub>CC</sub> UVLO	V <sub>CC-UVF</sub>	Falling	3.65	3.8	3.9	V
EXT LDO						
EXTVCC Operating Voltage Range			4.84		24	V
EXTVCC Switchover Threshold	EXTVCC	Rising	4.56	4.7	4.84	V
	EXTVCC	Falling	4.3	4.45	4.6	V
EXTVCC Dropout	EXTVCC_DO	EXTVCC = 4.75V, IV <sub>CC</sub> = 20mA			0.3	V
EXTVCC Current Limit	IV <sub>CC-MAX</sub>	V <sub>CC</sub> = 4.5V, EXTVCC = 7V	40	85	160	mA

## **Electrical Characteristics (continued)**

 $(V_{IN} = V_{EN/UVLO} = 24V, R_{RT} = 40.2K\Omega \ (f_{SW} = 500kHz), C_{VCC} = 10\mu\text{F}, V_{SGND} = V_{PGND} = V_{MODE/SYNC} = V_{EXTVCC} = 0V, V_{FB} = 1V, LX = SS = CF = \overline{RESET} = OPEN, V_{BST} \ to V_{LX} = 5V, T_{A} = -40^{\circ}\text{C} \ to 125^{\circ}\text{C}, unless otherwise noted. Typical values are at T_{A} = +25^{\circ}\text{C}.$  All voltages are referenced to SGND, unless otherwise noted.) (Note 3)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
POWER MOSFETS						
High-Side nMOS On-Resistance	R <sub>DS-ONH</sub>	I <sub>LX</sub> = 0.3A ,sourcing		100	200	mΩ
Low-Side nMOS On-Resistance	R <sub>DS-ONL</sub>	I <sub>LX</sub> = 0.3A , sinking		64	125	mΩ
LX Leakage Current	ILX <sub>LKG</sub>	$T_A = 25^{\circ}C$ , $V_{LX} = (V_{PGND} + 1V)$ to $(V_{IN} - 1V)$	-2		+2	μΑ
SOFT START					,	
Soft-Start Current	I <sub>SS</sub>	V <sub>SS</sub> = 0.5V	4.7	5	5.3	μΑ
FEEDBACK (FB)					,	
FB Regulation Voltage	V <sub>FB_REG</sub>	MODE/SYNC = SGND or V <sub>CC</sub>	0.892	0.9	0.908	V
FB Regulation Voltage	V <sub>FB_REG</sub>	MODE/SYNC = OPEN	0.892	0.916	0.934	V
FB Input Leakage Current	I <sub>FB</sub>	0 < V <sub>FB</sub> < 1V, T <sub>A</sub> = 25°C	-50		+50	nA
MODE/SYNC						
MODE Threshold	V <sub>M-DCM</sub>	MODE = V <sub>CC</sub> (DCM Mode)	V <sub>CC</sub> - 0.65			V
MODE Threshold	V <sub>M-PFM</sub>	MODE = OPEN (PFM Mode)		V <sub>CC</sub> /2		V
MODE Threshold	V <sub>M-PWM</sub>	MODE = SGND (PWM Mode)			0.75	V
SYNC Frequency Capture Range			1.1 x F <sub>SW</sub>		1.4 x F <sub>SW</sub>	kHz
SYNC Pulse Width			50			ns
CVNC Threehold	V <sub>IL</sub>				0.8	V
SYNC Threshold	V <sub>IH</sub>		2.1			V
CURRENT LIMIT			•			
Peak Current Limit Threshold	I <sub>PEAK-LIMIT</sub>		4.4	5.25	5.85	Α
Runaway Current Limit Threshold	I <sub>RUNAWAY</sub> - LIMIT		4.9	5.8	6.7	А
Valley Current-Limit Threshold	IVALLEY-LIMIT	MODE/SYNC = OPEN or MODE/ SYNC = V <sub>CC</sub>	-0.25	0	+0.25	А
Valley Current-Limit Threshold	I <sub>VALLEY-LIMIT</sub>	MODE/SYNC = SGND		-1.8		А
PFM Current-Limit Threshold	I <sub>PFM</sub>	MODE/SYNC = OPEN	0.575	0.725	0.9	Α

## **Electrical Characteristics (continued)**

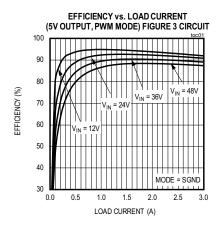
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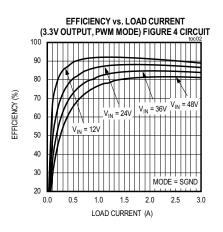
PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
RT/SYNC						
		R <sub>RT</sub> = 40.2KΩ	475	500	525	kHz
Switching Fragueno	-	R <sub>RT</sub> = OPEN	460	500	540	kHz
Switching Frequency	$F_{SW}$	R <sub>RT</sub> = 8.06KΩ	1950	2200	2450	kHz
		R <sub>RT</sub> = 210KΩ	90	100	110	kHz
V <sub>FB</sub> Undervoltage Trip Level to Cause HICCUP	V <sub>OUT-HICF</sub>		0.56	0.58	0.65	V
HICCUP Timeout				32768		Cycles
Minimum On-Time	ton_min			60	80	ns
Minimum off-Time	t <sub>OFF_MIN</sub>		140		160	ns
LX Dead Time				5		ns
RESET						
RESET Output Level Low		I <sub>RESET</sub> = 10mA			400	mV
RESET Output Leakage Current		$T_A = T_J = 25$ °C, $V_{\overline{RESET}} = 5.5$ V	-0.1		+0.1	μΑ
FB Threshold for RESET Deassertion	V <sub>FB-OKR</sub>	V <sub>FB</sub> rising	93.8	95	97.8	%
FB Threshold for RESET Assertion	V <sub>FB-OKF</sub>	V <sub>FB</sub> falling	90.5	92	94.6	%
RESET De-Assertion Delay After FB Reaches 95% Regulation				1024		Cycles
THERMAL SHUTDOWN			•			
Thermal Shutdown Threshold	T <sub>SHDNR</sub>	Temp rising		165		°C
Thermal Shutdown Hysteresis	T <sub>SHDNHY</sub>			10		°C

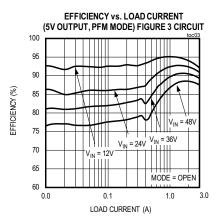
Note 3: All limits are 100% tested at  $T_A = +25^{\circ}C$ . Limits over the operating temperature range and relevant supply voltage range are guaranteed by design and characterization.

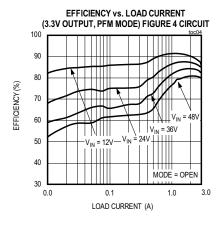
## **Typical Operating Characteristics**

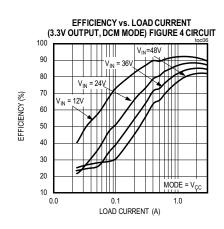
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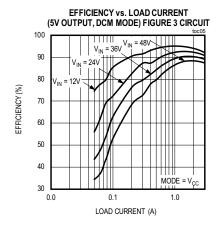


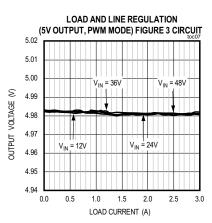






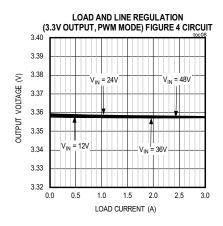


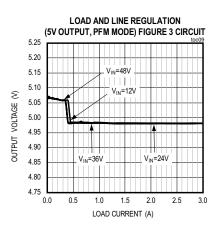


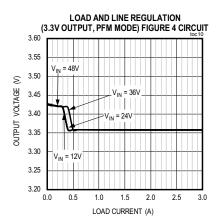


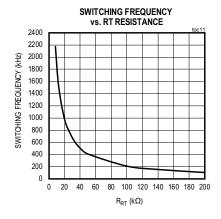
## **Typical Operating Characteristics (continued)**

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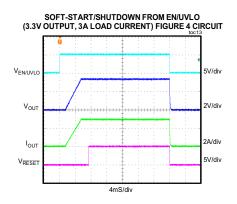


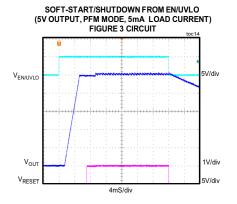






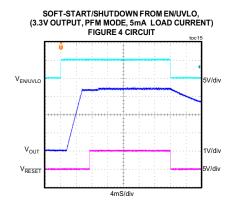


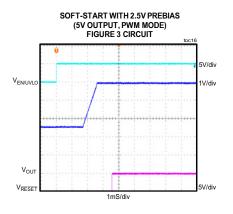


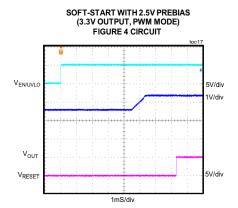


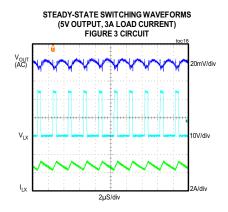
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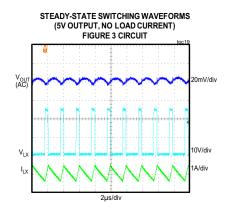
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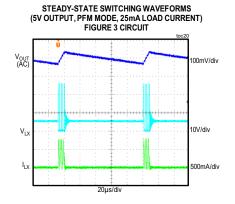






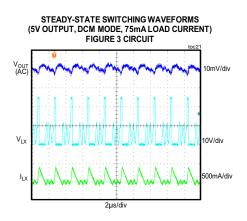


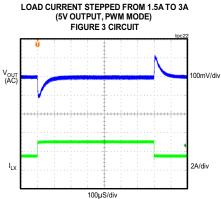


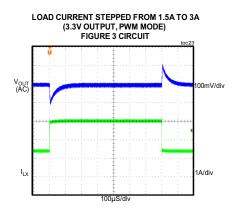


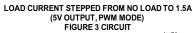
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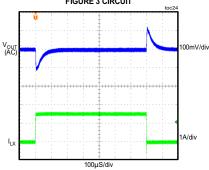
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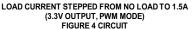


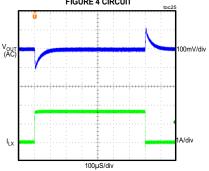




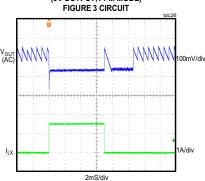




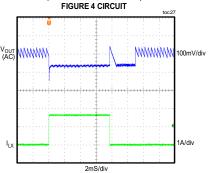




#### LOAD CURRENT STEPPED FROM 5MA TO 1.5A (5V OUTPUT, PFM MODE)

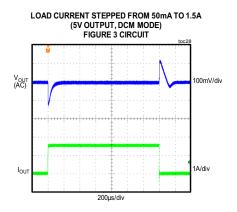


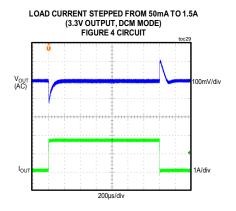
#### LOAD CURRENT STEPPED FROM 5mA TO 1.5A (3.3V OUTPUT, PFM MODE)

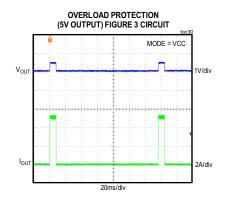


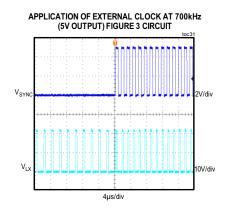
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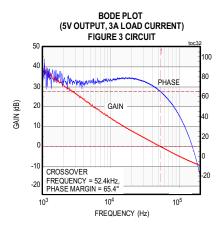
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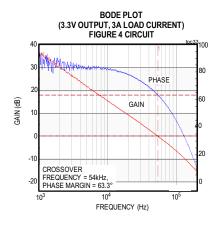




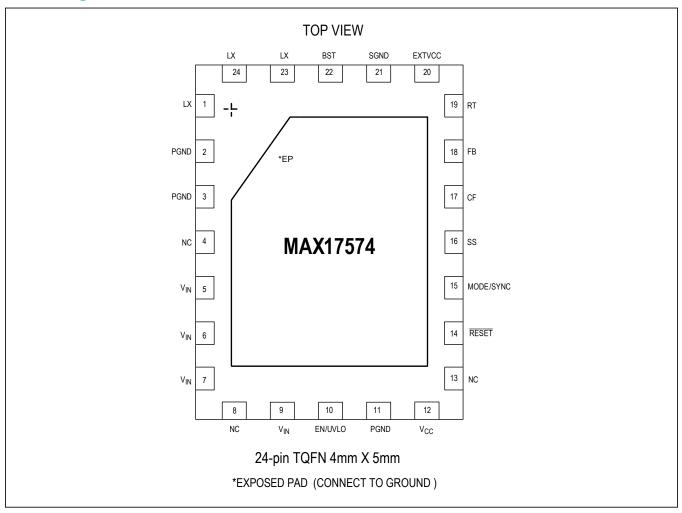








## **Pin Configuration**



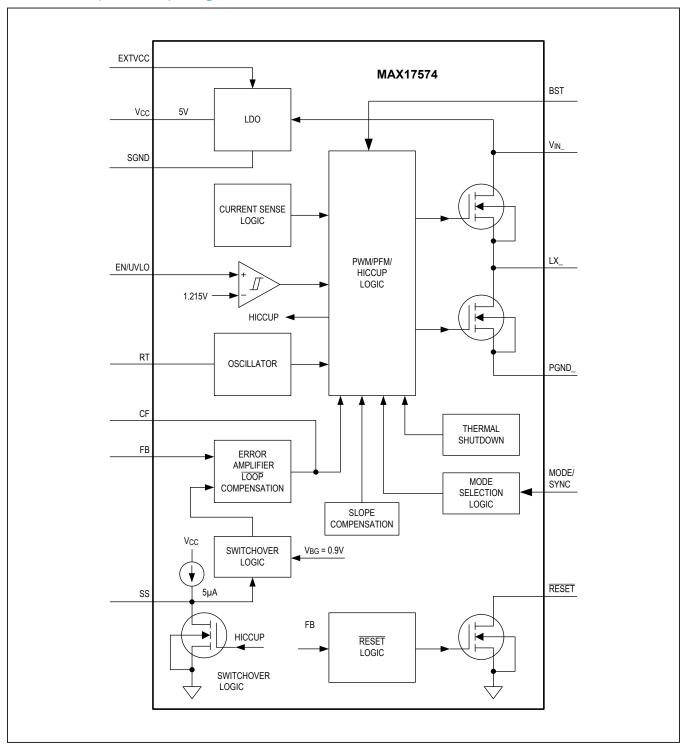
## **Pin Description**

NAME	PIN	FUNCTION
1, 23, 24	LX	Switching Nodes. Connect LX pins to the switching side of the inductor.
2, 3, 11	PGND	Power Ground Pins of the Converter. Connect externally to the power ground plane. Connect the SGND and PGND pins together at the ground return path of the V <sub>CC</sub> bypass capacitor. Refer to the <i>MAX17574 Evaluation Kit</i> data sheet for a layout example
4, 8, 13	N.C.	No Connect. Keep these pins open.
5–7, 9	$V_{IN}$	Power-Supply Input. The input supply range is from 4.5V to 60V.

# **Pin Description (continued)**

NAME	PIN	FUNCTION
10	EN/UVLO	Enable/Undervoltage Lockout Pin. Drive EN/UVLO high to enable the output. Connect to the center of the resistor-divider between $V_{\text{IN}}$ and SGND to set the input voltage at which the part turns on. Connect to $V_{\text{IN}}$ pins for always-on operation.
12	V <sub>CC</sub>	5V LDO Output of the Part. Bypass $V_{CC}$ with a $2.2\mu F/10V/X7R/0603$ ceramic capacitor to SGND in PWM and DCM modes, and $10\mu F/10V/X7R/0805$ ceramic capacitor in PFM mode.
14	RESET	Open-Drain RESET Output. The RESET output is driven low if FB drops below 92% of its set value. RESET goes high 1024 cycles after FB rises above 95% of its set value.
15	MODE/ SYNC	MODE pin configures the device to operate either in PWM, PFM, or DCM modes of operation. Leave MODE unconnected for PFM operation (pulse-skipping at light loads). Connect MODE to SGND for constant-frequency PWM operation at all loads. Connect MODE to V <sub>CC</sub> for DCM operation. The device can be synchronized to an external clock using this pin. See the <u>Mode Selection (MODE)</u> section and the <u>External Frequency Synchronization</u> section for more details.
16	SS	Soft-Start Input. Connect a capacitor from SS to SGND to set the soft-start time.
17	CF	At switching frequencies lower than 500kHz, connect a capacitor from CF to FB. Leave CF open if switching frequency is equal or more than 500kHz.
18	FB	Feedback Input. Connect FB to the center tap of an external resistor-divider from the output to SGND to set the output voltage. See the <i>Adjusting Output Voltage</i> section for more details
19	RT	Connect a resistor from RT to SGND to set the regulator's switching frequency between 100kHz and 2.2MHz. Leave RT open for the default 500kHz frequency. See the Setting the Switching Frequency (RT) section for more details.
20	EXTVCC	External Power Supply Input for the Internal LDO. Applying a voltage between 4.84V and 24V at EXTVCC pin will bypass the internal LDO and improve efficiency. Add a 4.7 $\Omega$ resistor from buck output to this pin to limit V <sub>CC</sub> bypass cap discharge current during output short-circuit condition. Also, add a local bypassing on this pin to SGND.
21	SGND	Analog Ground.
22	BST	Boost Flying Capacitor. Connect a 0.1µF ceramic capacitor between BST and LX.
_	EP	Exposed Pad. Connect to the GND pin of the IC. Connect to a large copper plane below the IC to improve heat dissipation capability.

## **Functional (or Block) Diagram**



### **Detailed Description**

The MAX17574, high-efficiency, high-voltage, synchronous step-down DC-DC converter with integrated MOSFETs operates over a 4.5V to 60V input. The converter can deliver up to 3A current. Output voltage is programmable from 0.9V to  $90\%V_{IN}$ . The feedback voltage regulation accuracy over -40°C to +125°C is ±0.9%.

The MAX17574 features a peak-current-mode control architecture. The device can be operated in the pulse-width modulation (PWM), pulse-frequency modulation (PFM) or discontinuous-conduction mode (DCM) control schemes. A programmable soft-start feature allows users to reduce input inrush current. The device also incorporates an output enable/under voltage lockout pin (EN/UVLO) that allows the user to turn on the part at the desired input voltage level. An open-drain RESET pin provides a delayed power-good signal to the system upon achieving successful regulation of the output voltage.

### Mode Selection (MODE)

The logic state of the MODE pin is latched when  $V_{CC}$  and EN/UVLO voltages exceed the respective UVLO rising thresholds and all internal voltages are ready to allow LX switching. If the MODE pin is open at power-up, the device operates in PFM mode at light loads. If the MODE pin is grounded at power-up, the device operates in constant-frequency PWM mode at all loads. Finally, if the MODE pin is connected to  $V_{CC}$  at power-up, the device operates in constant-frequency DCM mode at light loads. State changes on the MODE pin are ignored during normal operation.

#### **PWM Mode Operation**

In PWM mode, the inductor current is allowed to go negative. PWM operation provides constant frequency operation at all loads, and is useful in applications sensitive to switching frequency. However, the PWM mode of operation gives lower efficiency at light loads compared to PFM and DCM modes of operation.

#### **PFM Mode Operation**

PFM mode of operation disables negative inductor current and additionally skips pulses at light loads for high efficiency. In PFM mode, the inductor current is forced to a fixed peak of 725mA every clock cycle until the output rises to 102.3% of the nominal voltage. Once the output reaches 102.3% of the nominal voltage, both the high-side and low-side FETs are turned off and the device enters hibernate operation until the load discharges the output to 101.1% of the nominal voltage. Most of the internal blocks are turned off in hibernate

operation to save quiescent current. After the output falls below 101.1% of the nominal voltage, the device comes out of hibernate operation, turns on all internal blocks, and again commences the process of delivering pulses of energy to the output until it reaches 102.3% of the nominal output voltage. The advantage of the PFM mode is higher efficiency at light loads because of lower quiescent current drawn from supply. The trade-off is that the output-voltage ripple is higher compared to PWM or DCM modes of operation and switching frequency is not constant at light loads. The output voltage ripple in PFM mode can be reduced by increasing the amount of output capacitance.

#### **DCM Mode Operation**

DCM mode of operation features constant frequency operation down to lighter loads than PFM mode, by not skipping pulses but only disabling negative inductor current at light loads. DCM operation offers efficiency performance that lies between PWM and PFM modes.

### Linear Regulator (V<sub>CC</sub> and EXTVCC)

The MAX17574 has two internal LDO (Low Dropout) regulators which powers  $V_{CC}.$  One LDO is powered from  $V_{IN}$  (INLDO) and the other LDO is powered from EXTVCC (EXTVCC LDO). Only one of the two LDOs is in operation at a time, depending on the voltage levels present at EXTVCC. If EXTVCC voltage is greater than 4.7V (typ),  $V_{CC}$  is powered from EXTVCC. If EXTVCC is lower than 4.7V (typ),  $V_{CC}$  is powered from  $V_{IN}$ . Powering  $V_{CC}$  from EXTVCC increases efficiency at higher input voltages. EXTVCC voltage should not exceed 24V.

Typical  $V_{CC}$  output voltage is 5V. Bypass  $V_{CC}$  with a 2.2µF ceramic capacitor to SGND in PWM and DCM modes, and  $10\mu\text{F}/10\text{V}/\text{X7R}/0805$  ceramic capacitor in PFM mode. Recommended capacitor part number for  $10\mu\text{F}$  part is C2012X7R1A106K125AC (TDK).  $V_{CC}$  powers the internal blocks and the low-side MOSFET driver and re-charges the external bootstrap capacitor. Both INLDO and EXTVCC LDO can source up to 65mA. The MAX17574 employs an undervoltage lockout circuit that forces both the regulators off when  $V_{CC}$  falls below 3.8V (typ). The regulators can be immediately enabled again when  $V_{CC} > 4.2\text{V}$ . The 400mV UVLO hysteresis prevents chattering on power-up/power-down.

In applications where the buck converter output is connected to EXTVCC pin, if the output is shorted to ground then the transfer from EXTVCCLDO to INLDO happens seamlessly without any impact on the normal functionality.

#### **Switching Frequency Selection**

The switching frequency of the device can be programmed from 100kHz to 2.2MHz by using a resistor connected from the RT pin to SGND. The switching frequency ( $f_{SW}$ ) is related to the resistor connected at the RT pin ( $R_{RT}$ ) by the following equation:

$$R_{RT} = \frac{21 \times 10^3}{f_{SW}} - 1.7$$

where  $R_{RT}$  is in  $k\Omega$  and  $f_{SW}$  is in kHz. Leaving the RT pin open causes the device to operate at the default switching frequency of 500kHz. See <u>Table 1</u> for RT resistor values for a few common switching frequencies.

#### **External Frequency Synchronization**

The internal oscillator of the MAX17574 can be synchronized to an external clock signal on the MODE/SYNC pin. The external synchronization clock frequency must be between 1.1 x f<sub>SW</sub> and 1.4 x f<sub>SW</sub>, where f<sub>SW</sub> is the frequency programmed by the RT resistor. When an external clock is applied to MODE/SYNC pin, the internal oscillator frequency changes to external clock frequency (from original frequency based on RT setting) after detecting 16 external clock edges. The converter will operate in PWM mode during synchronization operation.

When the external clock is applied on-fly then the mode of operation will change to PWM from the initial state of PFM/DCM/PWM. When the external clock is removed on-fly then the internal oscillator frequency changes to the RT set frequency and the converter will still continue to operate in PWM mode. The minimum external clock pulse-width high should be greater than 50ns. See the MODE/SYNC section in the <u>Electrical Characteristics</u> table for details.

Table 1. Switching Frequency vs. RT Resistor

SWITCHING FREQUENCY (kHz)	RT RESISTOR $(k\Omega)$
500	OPEN
100	210
200	102
400	49.9
1000	19.1
1200	8.06

#### **Operating Input Voltage Range**

The minimum and maximum operating input voltages for a given output voltage should be calculated as follows:

$$\begin{split} V_{IN(MIN)} = & \frac{V_{OUT} + \left(I_{OUT(MAX)} \times (R_{DCR} + R_{DS-ONL})\right)}{D_{MAX}} \\ + & \left(I_{OUT(MAX)} \times (R_{DS-ONH} - R_{DS-ONL})\right) \\ V_{IN(MAX)} = & \frac{V_{OUT}}{f_{SW(MAX)} \times f_{ON(MIN)}} \end{split}$$

Where  $V_{OUT}$  is the steady-state output voltage,  $I_{OUT\ (MAX)}$  is the maximum load current,  $R_{DCR}$  is the DC resistance of the inductor,  $f_{SW(MAX)}$  is the maximum switching frequency,  $t_{OFF(MAX)}$  is the worst-case minimum switch off-time (160ns) and  $t_{ON-MIN}$  is the worst-case minimum switch on-time (80ns).

#### **Overcurrent Protection/Hiccup Mode**

The device is provided with a robust overcurrent protection scheme that protects the device under overload and output short-circuit conditions. A cycle-by-cycle peak current limit turns off the high-side MOSFET whenever the highside switch current exceeds an internal limit of 5.25A (typ). A runaway current limit on the high-side switch current at 5.8A (typ) protects the device under high input voltage, short-circuit conditions when there is insufficient output voltage available to restore the inductor current that was built up during the on period of the step-down converter. One occurrence of the runaway current limit triggers a hiccup mode. In addition, if, due to a fault condition, feedback voltage drops to 0.58V (typ) any time after soft-start is complete, and hiccup mode is triggered. In hiccup mode, the converter is protected by suspending switching for a hiccup timeout period of 32,768 clock cycles. Once the hiccup timeout period expires, soft-start is attempted again. Note that when soft-start is attempted under overload condition, if feedback voltage does not exceed 0.58V, the device switches at half the programmed switching frequency. Hiccup mode of operation ensures low power dissipation under output short-circuit conditions.

## **RESET Output**

The device includes a RESET comparator to monitor the output voltage. The open-drain RESET output requires an external pullup resistor. RESET goes high (high impedance) 1024 switching cycles after the regulator output increases above 95% of the designed nominal regulated voltage. RESET goes low when the regulator output voltage drops to below 92% of the nominal regulated voltage. RESET also goes low during thermal shutdown.

#### **Prebiased Output**

When the MAX17574 starts into a prebiased output, both the high-side and the low-side switches are turned off so that the converter does not sink current from the output. High-side and low-side switches do not start switching until the PWM comparator commands the first PWM pulse, at which point switching commences. The output voltage is then smoothly ramped up to the target value in alignment with the internal reference.

#### **Thermal Shutdown Protection**

Thermal shutdown protection limits total power dissipation in the device. When the junction temperature of the device exceeds +165°C, an on-chip thermal sensor shuts down the device, allowing the device to cool. The thermal sensor turns the device on again after the junction temperature cools by 10°C. Soft-start resets during thermal shutdown. Carefully evaluate the total power dissipation (see the <u>Power Dissipation</u> section) to avoid unwanted triggering of the thermal shutdown protection in normal operation.

### **Applications Information**

#### **Input Capacitor Selection**

The input filter capacitor reduces peak currents drawn from the power source and reduces noise and voltage ripple on the input caused by the circuit's switching. The input capacitor RMS current requirement ( $I_{RMS}$ ) is defined by the following equation:

$$I_{RMS} = I_{OUT(MAX)} \times \frac{\sqrt{V_{OUT} \times (V_{IN} - V_{OUT})}}{V_{IN}}$$

where,  $I_{OUT(MAX)}$  is the maximum load current.  $I_{RMS}$  has a maximum value when the input voltage equals twice the output voltage ( $V_{IN} = 2 \times V_{OUT}$ ), so  $I_{RMS(MAX)} = I_{OUT(MAX)}/2$ . Choose an input capacitor that exhibits less than +10°C temperature rise at the RMS input current for optimal long-tem reliability. Use low-ESR ceramic capacitors with high-ripple-current capability at the input. X7R capacitors are recommended in industrial applications for their temperature stability. Calculate the input capacitance using the following equation:

$$C_{IN} = \frac{I_{OUT(MAX)} \times D \times (1-D)}{\eta \times f_{SW} \times \Delta V_{IN}}$$

where D =  $V_{OUT}/V_{IN}$  is the duty ratio of the controller,  $f_{SW}$  is the switching frequency,  $\Delta V_{IN}$  is the allowable input voltage ripple, and  $\eta$  is the efficiency.

In applications where the source is located distant from the device input, an electrolytic capacitor should be added in parallel to the ceramic capacitor to provide necessary damping for potential oscillations caused by the inductance of the longer input power path and input ceramic capacitor.

#### **Inductor Selection**

Three key inductor parameters must be specified for operation with the device: inductance value (L), inductor saturation current ( $I_{SAT}$ ) and DC resistance ( $R_{DCR}$ ). The switching frequency and output voltage determine the inductor value as follows:

$$L = \frac{V_{OUT}}{f_{SW}}$$

Where  $V_{OUT}$  and  $f_{SW}$  are nominal values and  $f_{SW}$  is in Hz. Select an inductor whose value is nearest to the value calculated by the previous formula.

Select a low-loss inductor closest to the calculated value with acceptable dimensions and having the lowest possible DC resistance. The saturation current rating (I<sub>SAT</sub>) of the inductor must be high enough to ensure that saturation can occur only above the peak current-limit value of 5.25A.

#### **Output Capacitor Selection**

X7R ceramic output capacitors are preferred due to their stability over temperature in industrial applications. The output capacitors are usually sized to support a step load of 50% of the maximum output current in the application, so the output voltage deviation is contained to 3% of the output voltage change. The minimum required output capacitance can be calculated as follows:

$$\begin{split} C_{OUT} &= \frac{1}{2} \times \frac{I_{STEP} \times t_{RESPONSE}}{\Delta V_{OUT}} \\ &\quad t_{RESPONSE} \cong (\frac{0.33}{f_C} + \frac{1}{f_{SW}}) \end{split}$$

where I<sub>STEP</sub> is the load current step,  $t_{RESPONSE}$  is the response time of the controller,  $\Delta V_{OUT}$  is the allowable output-voltage deviation,  $f_C$  is the target closed-loop crossover frequency, and  $f_{SW}$  is the switching frequency. Select  $f_C$  to be 1/9th of  $f_{SW}$  if the switching frequency is less than or equal to 500kHz. If the switching frequency is more than 500kHz, select  $f_C$  to be 55kHz.

### Soft-Start capacitor selection

The device implements adjustable soft-start operation to reduce inrush current. A capacitor connected from the SS pin to GND programs the soft-start time. The selected output capacitance (C<sub>SEL</sub>) and the output voltage (V<sub>OUT</sub>) determine the minimum required soft-start capacitor as follows:

$$C_{SS} \geq 28 \times 10^{-6} \times C_{SEL} \times V_{OUT}$$

The soft-start time  $(t_{SS})$  is related to the capacitor connected at SS (C<sub>SS</sub>) by the following equation:

$$t_{SS} = \frac{C_{SS}}{5.55 \times 10^{-6}}$$

For example, to program a 1ms soft-start time, a 5.6nF capacitor should be connected from the SS pin to GND.

#### Setting the Input Undervoltage-Lockout Level

The device offers an adjustable input undervoltage-lockout level. Set the voltage at which the device turns on with a resistive voltage-divider connected from V<sub>IN</sub> to SGND. Connect the center node of the divider to EN/UVLO. (see Figure 1) Choose R1 to be  $3.3M\Omega$  and then calculate R2 as follows:

$$R2 = \frac{R1 \times 1.215}{(V_{INIL} - 1.215)}$$

**Table 2. C6 Capacitor Value at Various** Switching Frequencies

SWITCHING FREQUENCY RANGE (kHz)	C6 (pF)
200 to 300	2.2
300 to 400	1.2
400 to 500	0.75

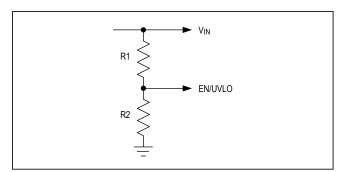


Figure 1. Setting the Input Undervoltage Lockout

where V<sub>INI I</sub> is the voltage at which the device is required to turn on. Ensure that  $V_{INU}$  is higher than 0.8 x  $V_{OUT}$ .

#### **Loop Compensation**

The device is internally loop compensated. However, if the switching frequency is less than 500kHz, connect a 0402 capacitor C6 between the CF pin and the FB pin. Use Table 2 to select the value of C6.

### **Adjusting Output Voltage**

Set the output voltage with a resistive voltage-divider connected from the positive terminal of the output capacitor (VOLIT) to SGND (see Figure 2). Connect the center node of the divider to the FB pin. Use the following procedure to choose the resistive voltage-divider values:

Calculate resistor R6 from the output to the FB pin as follows:

$$R6 = \frac{216 \times 10^3}{f_C \times C_{OUT}}$$

where R6 is in  $k\Omega$ , crossover frequency  $f_C$  is in kHz, and the output capacitor  $C_{OUT}$  is in  $\mu F$ . Choose  $f_C$  to be 1/9th of the switching frequency, f<sub>SW</sub>, if the switching frequency is less than or equal to 500kHz. If the switching frequency is more than 500kHz, select f<sub>C</sub> to be 55kHz. Calculate resistor R7 from the FB pin to SGND as follows:

$$R7 = \frac{R6 \times 0.9}{(V_{OLIT} - 0.9)}$$

R7 is in  $k\Omega$ .

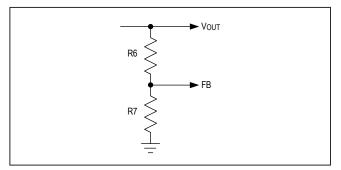


Figure 2. Adjusting Output Voltage

#### **Power Dissipation**

At a particular operating condition, the power losses that lead to temperature rise of the part are estimated as follows:

$$P_{LOSS} = (P_{OUT} \times (\frac{1}{\eta} - 1)) - (I_{OUT}^{2} \times R_{DCR})$$

$$P_{OUT} = V_{OUT} \times I_{OUT}$$

Where  $P_{OUT}$  is the output power,  $\eta$  is the efficiency of the converter and  $R_{DCR}$  is the DC resistance of the inductor (see the <u>Typical Operating Characteristics</u> for more information on efficiency at typical operating conditions).

For a typical multilayer board, the thermal performance metrics for the package are given below:

$$\theta_{JA} = 24^{\circ}C / W$$
  
 $\theta_{JC} = 1.8^{\circ}C / W$ 

The junction temperature of the device can be estimated at any given maximum ambient temperature  $(T_{A\_MAX})$  from the following equation:

$$T_{J\_MAX} = T_{A\_MAX} + (\theta_{JA} \times P_{LOSS})$$

If the application has a thermal-management system that ensures that the exposed pad of the device is maintained at a given temperature (TEP\_MAX) by using proper heat sinks, then the junction temperature of the device can be estimated at any given maximum ambient temperature as:

$$T_{J\_MAX} = T_{EP\_MAX} + (\theta_{JC} \times P_{LOSS})$$

Junction temperatures greater than +125°C degrades operating lifetimes.

#### **PCB Layout Guidelines**

All connections carrying pulsed currents must be very short and as wide as possible. The inductance of these connections must be kept to an absolute minimum due to the high di/dt of the currents. Since inductance of a current carrying loop is proportional to the area enclosed by the loop, if the loop area is made very small, inductance is reduced. Additionally, small-current loop areas reduce radiated EMI.

A ceramic input filter capacitor should be placed close to the  $V_{IN}$  pins of the IC. This eliminates as much trace inductance effects as possible and gives the IC a cleaner voltage supply. A bypass capacitor for the  $V_{CC}$  pin also should be placed close to the pin to reduce effects of trace impedance.

When routing the circuitry around the IC, the analog small-signal ground and the power ground for switching currents must be kept separate. They should be connected together at a point where switching activity is at a minimum, typically the return terminal of the  $V_{CC}$  bypass capacitor. This helps keep the analog ground quiet. The ground plane should be kept continuous/unbroken as far as possible. No trace carrying high switching current should be placed directly over any ground plane discontinuity.

PCB layout also affects the thermal performance of the design. A number of thermal throughputs that connect to a large ground plane should be provided under the exposed pad of the part, for efficient heat dissipation.

For a sample layout that ensures first pass success, refer to the MAX17574 evaluation kit layout available at <a href="https://www.maximintegrated.com">www.maximintegrated.com</a>.

## **Typical Application Circuits**

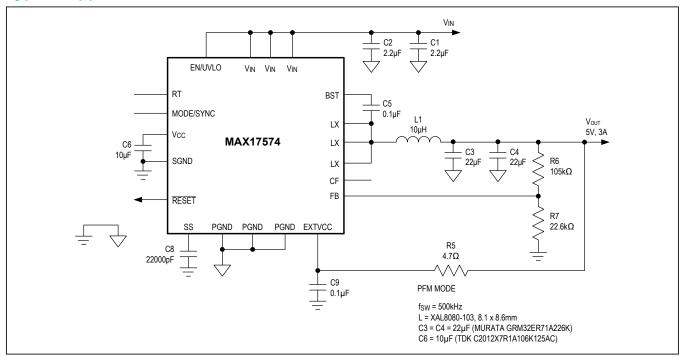


Figure 3: 5V Output Application Circuit

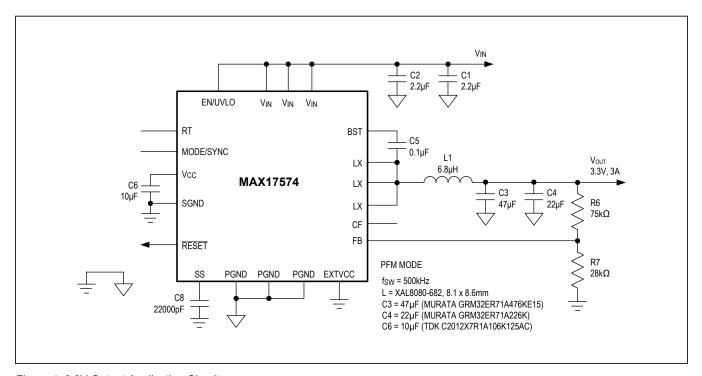


Figure 4: 3.3V Output Application Circuit

## MAX17574

4.5V to 60V, 3A, High-Efficiency, Synchronous Step-Down DC-DC Converter with Internal Compensation

# **Ordering Information**

PART	PIN-PACKAGE	PACKAGE-SIZE
MAX17574ATG+	24-TQFN EP*	4mm x 5mm

<sup>+</sup>Denotes a lead(Pb)-free/RoHS-compliant package. \*EP = Exposed pad.

## **Chip Information** PROCESS: BICMOS

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### MAX17574

# 4.5V to 60V, 3A, High-Efficiency, Synchronous Step-Down DC-DC Converter with Internal Compensation

## **Revision History**

REVISION NUMBER	REVISION DATE	DESCRIPTION	PAGES CHANGED
0	9/16	Initial release	_
1	7/17	Updated <i>Absolute Maximum Ratings</i> section and Package Thermal Characteristics in <i>Package Information</i> table. Updated <i>Electrical Characteristics</i> and <i>Typical Operating Characteristics</i> global conditions, and <i>Pin Description</i> table for Pin 12. Corrected typo in <i>Pin Description</i> table Pin 15. Updated <i>Linear Regulator</i> ( <i>V<sub>CC</sub></i> and <i>EXTVCC</i> ) section, equations in <i>Operating Input Voltage Range</i> and <i>Power Dissipation</i> sections, and <i>Typical Application Circuits</i> .	2–9, 11, 13–14, 16–19

For pricing, delivery, and ordering information, please contact Maxim Direct at 1-888-629-4642, or visit Maxim Integrated's website at www.maximintegrated.com.

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